

Control of a Nonlinear Tank Process using Dynamic Matrix Controller

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Abstract. The level process is widely used in many process industries for storing the liquids for mixing purpose in sugar mills, as settling tank and for water treatment plants. Most of the chemical plants are multivariable processes which exhibit nonlinear behaviour due to the existence of interactions between the input and output variables. The level control of the cylindrical tank is difficult because of its nonlinearity. Linear PID (Proportional Integral Derivative) controllers are generally used in many industrial control systems because of its simple structure and robustness, but when it comes to the control of nonlinear and multivariable processes, the controller parameters have to be continuously adjusted in order to deal with the nonlinearities, uncertainties and interaction between the variables. The major objective of this work is to control the level of a nonlinear tank process. This is achieved by modelling a nonlinear controller which can adapt to the nonlinear performance of the process. To achieve this goal, the mathematical modelling of a tank process is obtained. Dynamic Matrix Control (DMC) Controller is designed using the mathematical model to control the tank system. The performance of the controller can be analyzed through extensive simulation studies.

Keywords: DMC, PID.

1 Introduction

The control algorithm is quite complicated for the MIMO system due to variation in process dynamics that occurs due to changes that occur in the operating point and the characteristics of nonlinear dynamic coupling. Most of the real time systems are found to be nonlinear. The Tank Level System is widely used in many process industries for storing the liquids. Most of the chemical plants are multivariable processes which exhibit nonlinear behaviour due to the existence of interactions between the input and output variables. The level control of the cylindrical tank is difficult because of its nonlinearity.

The Model Predictive Control is used to compute the control signal which best corresponds to some standard that predicts the system behaviour. MPC is widely used for a long time in process industries. MPC has established itself in industries as an important form of advanced multivariable control. The use of MPC algorithm is used from early 1970's. The first MPC algorithm designed was Model Predictive Heuristic Control in 1976 by Richalet *et al*, and Cutler and Remaker in 1979 proposed Dynamic Matrix Control (DMC), the control outputs were calculated by applying the principle of receding horizon. DMC is designed for the control of level for the two conical tank interacting system and being implemented for the

same [1]. Takagi Sugeno fuzzy expert model based soft fault diagnosis for two tank interacting system from where the mathematical model is obtained [2].

A nonlinear Hammerstein-Wiener model predictive controller based on LSSVM is built to describe the dynamic characteristic of a continuous stirred tank reactor (CSTR) from [3]. The MPC algorithm is being designed for the mathematical model of the coupled tank system, which is a Multiple Input Multiple Output (MIMO) system on a flow controller valve. Dynamic Matrix Control (DMC) of Quadruple-Tank Process, which deals with the Model Predictive Control (MPC) known as DMC applied to a non linear multivariable laboratory for interacting tank systems [5-7].

2 Nonlinear system Description

Cylindrical tanks are broadly used in industries for storing the liquids (kerosene, petrol, water, diesel etc.), mixing purpose in sugar mills, reactors for mass chemicals separation, as settling tank and as well as for water treatment plants. While most of the chemical plants are multivariable processes which reveal nonlinear behaviour due to the continuation of interactions between input and output variables. The control of these processes is a exigent task when compared to SISO processes.

The schematic diagram of the nonlinear tank process set-up is shown in Fig.1. It consists of a cylindrical. The pneumatic control valves fine-tune the flow of water pumped from the reservoir into the tanks (F_{in}). Rotameters are set at the inlet the tank to measure the inflow of the tank. The tank is provide with a Differential Pressure Transmitter (DPT) to measure the pressure of the liquid column and transformed into the water level.

The discharge flow of the tank is shown in the dynamic model, the inward mass flows F_{in} are defined as inputs, while the measurements $H(t)$ the height of fluid in tank are considered as output. The dynamic model is derived using the inward and extrovert mass flows and is described by the following differential equation (1) which is obtained from [2].

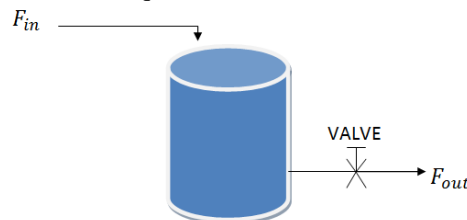


Fig 1 Nonlinear Cylindrical Tank System

3 Mathematical Model Of Nonlinear Cylindrical Tank System

The equation of the Nonlinear Tank process is givenby,

$$A \frac{dh}{dt} = F_{in} - b\sqrt{h} \quad (1)$$

$$b = s. a. \sqrt{2g} \quad (2)$$

Table 1 Parameters of cylindrical tank system

S.No.	Description	Value
1	Area of the tanks (A)	0.0154 m ²
2	Acceleration due to gravity (g)	9.81 m/ sec ²
3	Maximum permissible height of water levels (h max)	0.63 m
4	Cross section of the connecting pipes (a)	0.005 m ²
5	Co-efficient of the connecting pipes(s)	0.45
6	Nominal operating condition h = 0.4 (m)	Nominal inflow rate $Fin_1 = 0.00315m^3 / sec$

The transfer function for tank obtained from the above parameters is given as,

$$\frac{H(s)}{F_{in}(s)} = \frac{1.2693}{1.954s + 1} \quad (3)$$

4 Dmc Controller Design

The Model Predictive Control is the backbone of Dynamic Matrix Control. In this controller, the model which is used determines the behaviour of complex dynamical systems. The nonlinearities in the process and the complexity are due to non-coherent process degeneration. Hence, the process model predicts the behaviour of the outputs of the modelled dynamic system based on the process input changes. In this controller the transfer function needs to be specified in order. The designing is first based on the step response which is given in the form,

$$\hat{Y}_k = \sum_{i=1}^N s_i \Delta u_{k-i} + s_N u_{k-N} \quad (4)$$

The past control moves and the future control moves are separated by the following equation,

$$\hat{Y}_k = s_1 \Delta u_{k+j-1} + s_2 \Delta u_{k+j-2} + \dots + s_j \Delta u_k + s_N \Delta u_{k-N-j}$$

$$+s_{j-1}\Delta u_{k-1} + s_{j+1} + s_{N-1}\Delta u_{k-N+j+2}(5)$$

A control horizon of M steps and a prediction horizon of P steps, are written in matrix-vector form, using matrix-vector notation.

$$\hat{Y}_c = s_f \Delta u_f + s_{past} \Delta u_{past} + s_N u_p + \hat{d} \quad (6)$$

The forced response and the free response which for forced response corresponds to the current and future control moves contributions and for free response that corresponds to the prediction of changes in output if there are no future control moves. Hence the minimized solution for this objective function is given as,

$$\Delta u_f = (s_f^T s_f + w)^{-1} s_f^T E(7)$$

$$\Delta u_f = k_1 E(8)$$

The equation (8) the represents the first row of the K matrix which is taken from [8].

Hence from these equations, the DMC is designed for the process model. The unforced error vector (E) is proportional to the present and future control move vector (Δu_f). In example, a controller gain matrix, K, multiplied with the unforced error vector. The first row of the K matrix based on the equation (8) is used as only the present control move is considered.

5 Simulation Results

Linearization is usually done for the system that is being non-linear to obtain the characteristic linear form of equation.

The tank process of the system is been linearized by Taylor Series for the tank equation. The Taylor series for the equation (1) of the tank process is been linearized and the transfer function is been obtained as shown in equation (3) and the Taylor series for the system to be obtained because the steady state point of operation. The equation (9) is a nonlinear equation and hence it needs to be linearized. Hence, in order to linearize the nonlinear term of the equation (1), Taylor series expansion is carried out as the following:

$$\sqrt{h} = \sqrt{h_s} + \frac{1}{2\sqrt{h_s}}(h) \quad (9)$$

The closed loop response of the tank process is obtained using the DMC are discussed below.

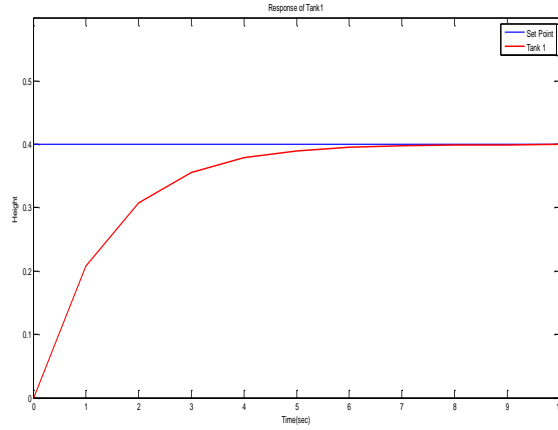


Fig.2 Closed Loop Response of Tank with P=5, N=25

The closed-loop response at set point $h = 0.4$ m; prediction horizon, $P = 5$; control horizon, $M = 1$; no weighting on inputs and model length, $N = 25$ is shown in the Fig.2. The response is reached at a nominal speed.

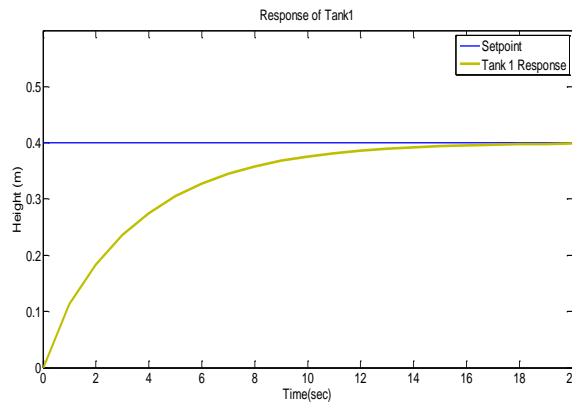


Fig 3 Closed loop response of Tank with P = 50, N = 100

The closed-loop response at set point $h = 0.4$ m; prediction horizon, $P = 50$; control horizon, $M = 1$; no weighting on inputs and model length, $N = 100$ is shown in the Fig.3.

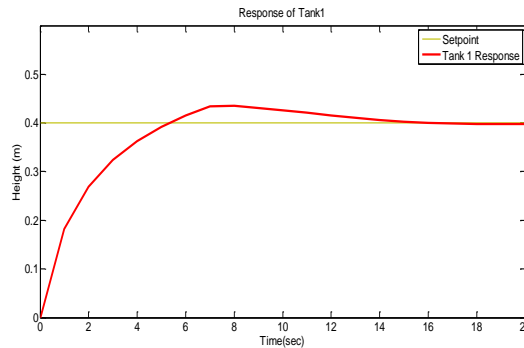


Fig.4 Closed loop response of Tank with $P = 5$, $N = 6$

The closed-loop response at set point $h = 0.4$ m; prediction horizon, $P = 5$; control horizon, $M = 1$; no weighting on inputs and model length, $N = 6$ is shown in the Fig.4. The response is obtained with some deviation.

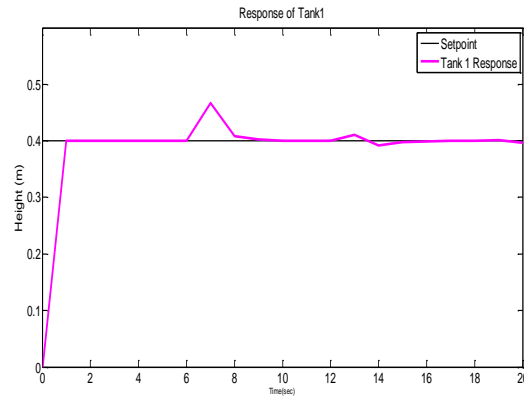


Fig.5 Closed loop response of Tank with $P = 1$, $N = 6$

The closed-loop response at set point $h = 0.4$ m; prediction horizon, $P = 1$; control horizon, $M = 1$; no weighting on inputs and model length, $N = 6$ is shown in the Fig.5. The response is obtained with some overshoot after few seconds.

6 Conclusion And Future Work

The design of DMC was done using MATLAB and response for a first order system was obtained with different values of Model Length (N), Control horizon (M) and Prediction horizon (P). The P should be lower than N otherwise the response reaches the steady state slowly. The same controller design was carried for the Tank process and the different values of P and N was given for the unit M value but with no weighting. It was observed that the P having higher value gives a slower settling time and the from the model length, it is observed that for lower values of N does not capture the process dynamics completely and thereby resulting in poor performance.

In future, the two-tank nonlinear interacting system can be carried out as a future work using DMC by selecting appropriate prediction horizon, control horizon and the model length. Then this work can be extended to the real time process.

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