

Study of Surface Topography of CW004A Copper after PWJ Disintegration

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Abstract. Presented article is focused on CW004A copper surface topography evaluation disintegrated using pulsed water jet enhanced by ultrasound. Primary objective was identification and describing of disintegration pulsed water jet areas effect on material with usage of round orifice nozzle. Twenty-five samples were manufactured with variable traverse feed speed $v_f = 0.1 - 20.0 \text{ mm.s}^{-1}$, to observe and assess areas of disintegration. Surface topography signs were evaluated using surface roughness parameters R_z [μm], R_p [μm], R_v [μm], mass material removal Δm [mg.mm^{-1}] and volume material removal V_m [mm^3]. As a result of experimental research were determined three basic areas of pulsating water jet effects on disintegrated surface.

Keywords: topography, copper, pulsating water jet, surface roughness

1 Introduction

Water's destructive effect on different materials is commonly known from history. First time water was used for manufacturing at the start of 20th century by Cook [1]. Currently, continual water jet (WJ) and abrasive water jet (AWJ [2], [3]) are generally used for disintegration of a wide range of materials. Using water jets with high-pressure reaches economic and technical limitations. Nowadays, there is a tendency for disintegration of material using lower pressure enhanced by additional gear, which characterizes pulsed water jet (PWJ). PWJ finds its purpose in many areas of industry, where dangerous conditions can occur. Dangerous conditions can cause damage, for example due to aggressive environments, increasing operation costs, ineffectiveness, exposure of adverse substances into the environment and the threat to life and health of people. These problems can be solved by replacing the current technological process by pulsed liquid jet. Many efforts to obtain non-continual liquid flow were recorded.

Continual jet modulation created by ultrasonic oscillation with additional gear – ultrasonic transducer was applied in the presented experimental work. The principle of enhanced pulse formation (Figure 1.) is based on vibrations forming in the ultrasonic transducer, which are transmitted into the fluid by usage of ultrasound guide and the ultrasound tool. Fluid jet exits the nozzle as a continual jet and in a specific distance begins forming clusters of water. Subsequently, the material is disintegrated by the effect of water clusters' impact with the high kinetic

energy. Magneto-strictive and piezo-electric transducers are used for creation of oscillation. [4], [5]

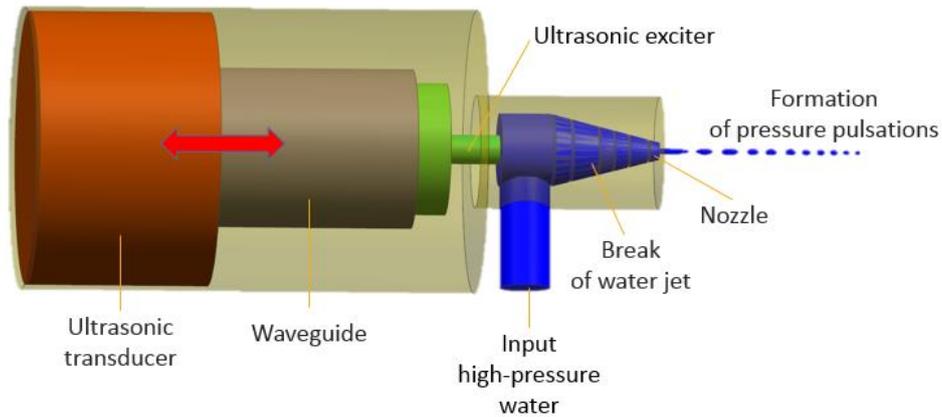


Fig. 1. Principle of ultrasound excited PWJ

Many researchers are concerned on liquid jet modulation and options of transfer pressure vibrations, for example *Puchala, et al.* [6], *Vijay* [7], [8], *Foldyna, et al.* [4], *Foldyna & Švehla* [9] and *Riha & Foldyna* [5].

Currently are some PWJ applications applied in practice, for example rock disintegration [8], renovation of the concrete structures [10], [11], surface treatment of the ornamental stones [12], for removal of burs and rust [13]. PWJ finds its application in human medicine to dental hygiene [14], in orthopedics and traumatology [15] and in the field of dermal medicine [16]. Micro pulsed water jet is applicable in the field of electronics, where is PWJ applied for microchips cooling [17].

Main objective of presented paper is describing PWJ disintegration efficiency with round nozzle and studying of new created surfaces with change of the traverse speed v [$\text{mm}\cdot\text{s}^{-1}$]. Experimental research continues in research [18], [19] where PWJ static effect was described.

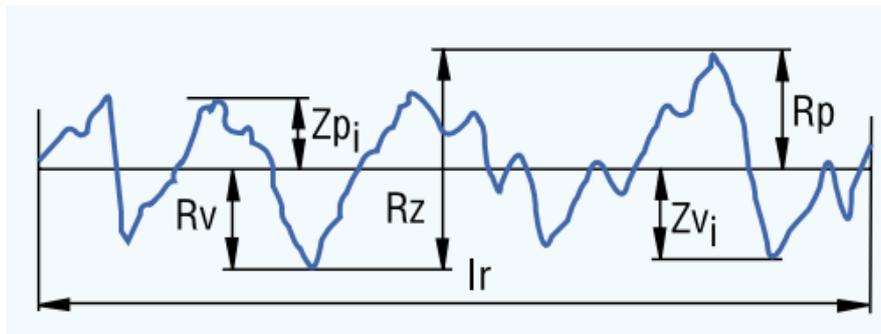


Fig. 2. Surface roughness parameters according to EN ISO 4287, where: Rz [μm] – maximal height of profile, Rv [μm] – maximal profile valley deep, Rp [μm] – maximal profile peak height, Zvi [μm] – profile valley deep, Zpi [μm] – profile peak height, lr [μm] – lenght [24]

Efficiency of disintegration was assessed using on Rz [μm], Rp [μm], Rv [μm] surface roughness parameters [25], [26] (Figure 2.), mass Δm [$\text{mg}\cdot\text{mm}^{-1}$] and volume material removal

V_m [mm³]. Surface roughness parameters belong to main topographic characteristics of the surface.

Experimental research presented in this work follows results of authors *Foldyna, et al.* [20], *Lehocka, et al.* [22], [23], [27], [28] and *Klich, et al.* [21].

Experiments were conducted in collaboration between FMT with a seat in Presov and Institute of Geonics of the CAS in Ostrava. Research samples were manufactured in Institute of Geonics of the CAS in Ostrava.

2 Set up of experiment

Cooper CW004A (Table 1.) was selected as experimental material. Basic properties of CW004A are high electric and thermal conductivity, resistance to corrosion

Experiment procedure was held using cutting head, circular orifice nozzle StoneAge wit, hydraulic high pressure pump Hammelmann HDP 253 (maximal operational pressure 160 MPa, maximal flow rate 67 l.min⁻¹), ultrasound gear Ecoson WJ-UG_630-40 and industrial robot ABB IRB 6640 - 180/2.55.

Table.1. Chemical composition, mechanical and physical properties of CW004A copper

Chemical composition [%]				
Cu + Ag			O	
> 99.90			< 0.04	
Mechanical properties				
Tensile strength R_m [MPa]	Yield strength $R_{p0.2}$ [MPa]	Min. elongation $L_0 = 100$ mm A [%]		Hardness HB/HV
395	365	4		114/120
Physical properties				
Density ρ [kg.m ⁻³]	Electrical resistivity ρ [$\Omega\mu$.m]	Thermal conductivity at 20°C λ [W.m ⁻¹ .K ⁻¹]	Elastic modulus at 20°C E [GPa]	Specific heat at 20°C C_p [J.kg ⁻¹ .K ⁻¹]
8 890	0.017 – 0.0178	388	115	380

25 experimental samples were prepared with rectangular shape and dimensions (l x w x t) (50x20x5 mm). Samples were produced using process conditions listed in Table 2. Variable condition was selected traverse speed v [mm.s⁻¹].

Every experimental sample was weighted before and after manufacturing using MettlerToledo PL303-ICweight. Mass material removal Δm [mg.s⁻¹] (Table 2.) was subsequently was calculated.

Topography measurement was realized using optical MicroProf FRT. Topography characteristics (profile, shape, and R_z [μ m], R_p [μ m], R_v [μ m] roughness) and volume material removal V_m [mm³] were assessed in software SPIP.

Table 2. Technological conditions of disintegration for changing traverse speed v [mm.s⁻¹]

Disintegration technological conditions					
d [mm]	p [MPa]	z [mm]	f [kHz]	P [W]	v [mm.s ⁻¹]
1.321	39	35	20.31	340	0.1 – 20.0

3 Evaluation of experiment

PWJ is composed of liquid pulses. Material is disintegrated and coextruded by pulse effect. The particles on material surface are segregated. Radial propagation of flow remove peaks and increase rate of material removal. With increasing exposition time is erosion effect more significant.

New created surface can be categorized into three effect areas of PWJ effect (Figure 3. – 5.):

1. Mass material removing area ($v = 0.1 - 7.0 \text{ mm.s}^{-1}$)
2. Surface roughening area ($v = 7.0 - 12.0 \text{ mm.s}^{-1}$)
3. Surface peening area ($v = 12.0 - 20.0$ and more mm.s^{-1})

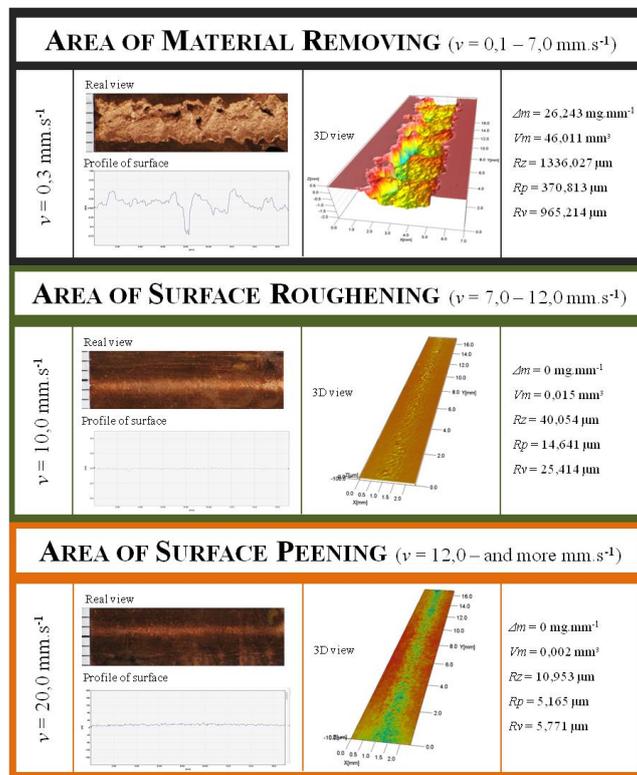


Fig. 3. Distribution of PWJ effects on disintegrated surface in accordance to traverse speed v [mm.s^{-1}] changes

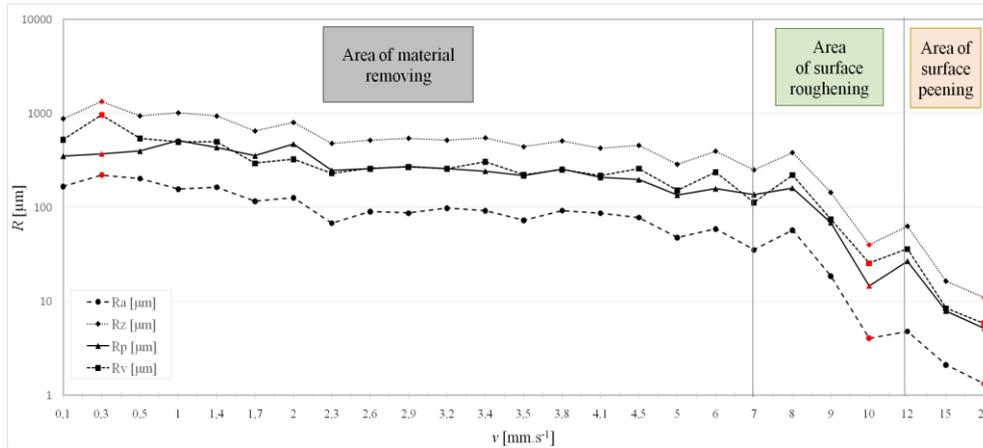


Fig. 4. Graphical dependence of PWJ erosion effects on change of roughness parameters Rz [μm], Rp [μm], Rv [μm]

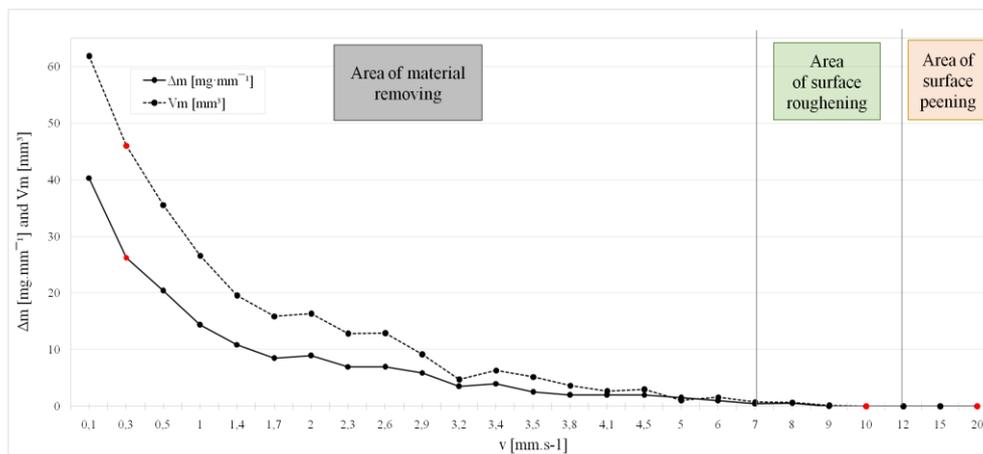


Fig. 5. Graphical dependence of PWJ erosion effects on change of mass Δm [$\text{mg}\cdot\text{mm}^{-1}$] and volume Vm [mm^3] material removal

1. Material removing area $v = 0.1 - 7.0 \text{ mm}\cdot\text{s}^{-1}$ (for illustration – Figure 3.; groove disintegrated with using traverse speed $v = 0.3 \text{ mm}\cdot\text{s}^{-1}$)

First area (area of the material removing) is characterized by intense erosive effect and significant changes of e topography. Impacting pulse with high-pitched kinetic energy disrupt surface and extrude volume of the material above surface. Subsequently radial flow amplified by repeated impact of the water clusters driven removed particles of the material and tears and cut surface. Deep and visible groove is created in eroded surface (Figure 3.). The groove is characteristic by uneven valleys and peaks with big height differences ($Rz = 396 - 1336 \mu\text{m}$, $Rp = 135 - 516 \mu\text{m}$, $Rv = 965 - 151 \mu\text{m}$). Erosion pores are formed in eroded groove, which spreads and create erosive craters. Mass ($\Delta m = 1 - 40 \text{ mg}\cdot\text{mm}^{-1}$) and volume ($Vm = 1 - 61 \text{ mm}^3$) material removal was significant for all samples in area of material removing. (Figure 4., 5.)

The erosion activity observed in the material removing area can be applied in industry fields to remove of large layers of the material, revitalization of the concrete structures and surface treatment of the ornamental stones.

2. Surface roughening area $v = 7.0 - 12.0 \text{ mm.s}^{-1}$ (shown on – Figure 3.; groove manufactured by the usage traverse speed $v = 10.0 \text{ mm.s}^{-1}$)

Second area (surface roughening zone) is characterized by pulses effect on the surface in shorter time interval. The radial flow of water does not create erosion effect, due to sort exposition time. In second area are not created deep craters. Mass material removal ($\Delta m = 0.0 - 0.5 \text{ mg.mm}^{-1}$) and volume material removal ($Vm = 0.01 - 0.7 \text{ mm}^3$) is very low, respectively is not observed (Figure 5.). Surface topography changes are described by creation of small valleys ($Rv = 25.0 - 220 \text{ }\mu\text{m}$) and peaks ($Rp = 15.0 - 161\mu\text{m}$) (Figure 4.). Surface quality is higher than in first area (area of material removing) (Figure 3.).

Mentioned effects of second area can be applied in the industry for preparation before surface treatment, cleaning and surface roughening.

3. Surface peening area $v = 12.0 - 20.0$ and more mm.s^{-1} (shown on – Figure 3.; groove disintegrated with using traverse speed $v = 20.0 \text{ mm.s}^{-1}$)

Third area (surface peening) is characterized by zero erosion effect on materials surface $\Delta m = 0 \text{ mg.mm}^{-1}$; $Vm = 0,003 \text{ mm}^3$ (Figure 5.). Pulsating water jet transmits too low energy for the surface disintegration. Surface craters were not observed, but very low level deformation effect occurred. Low deformation effect is characterized by the roughness parameters ($Rz = 10.9 - 16.3 \text{ }\mu\text{m}$) (Figure 4.). Compared to the values of roughness observed in unaffected area were $Rz = 5.48 \text{ }\mu\text{m}$; $Rp = 2.10 \text{ }\mu\text{m}$; $Rv = 3.38 \text{ }\mu\text{m}$.

The surfaces created with described process parameters can be applied for meliorate of utility properties of materials. Compressive residual stresses in the surface layer increase resistance to micro-cracks and thus increase durability of products.

4 Conclusion

Presented article defines different topographies created by pulsating water jet on CW004A copper surface and assesses different areas of PWJ effect. Based on experimental research can be concluded, that changes in PWJ efficiency can be observed with increasing of traverse speed [mm.s^{-1}].

PWJ effects on material can be divided into three areas:

1. Material removing area
2. Surface roughening area
3. Surface peening area

First area (area of material removing) can be used in many industrial fields to remove large layers or volumes of material, renovation of concrete structures and treatment of ornamental stone. Second area (surface roughening) can find its application in cleaning and roughening of surface before surface treatment. Third area (surface peening) is characterized by creation of compressive stress in material and can be applied in residual stress elimination and increase resistance to micro cracking. Surface treatment by peening can be used for higher durability under cyclic load.

Erosion effect of PWJ depends on exposition time and force affecting material surface. Presented experimental study described possibility of regulating and influencing pulsed liquid jet disintegration efficiency for changing traverse feed speed v [$\text{mm}\cdot\text{s}^{-1}$].

Traverse feed speed v [$\text{mm}\cdot\text{s}^{-1}$] straight influence exposition time of pulsating liquid jet and workpiece and change amount of impacts on the surface. Researchers *Brunton & Thomas* [18] and *Foldyna, et al.*, [19] presented significance of impact count on disintegration efficiency. It was proven that efficiency of disintegration increase when increase count of impacts. Research presented in this article confirms conclusions in [19] and identified new areas of investigation.

Regulation of PWJ efficiency can be reached by various settings of the technological set-up and process factors. Nowadays are primary regulation factors shape of nozzle orifice, lower pressures, the ultrasonic frequency modulation and optimal stand-off distance. Effect of erosion is also primary dependent on mechanical properties of material

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