Sliding Mode Controller Design for the Global Chaos Synchronization of Coullet Systems

Sundarapandian Vaidyanathan¹ and Sivaperumal Sampath²

R & D Centre, Vel Tech Dr. RR & Dr. SR Technical University Avadi-Alamathi Road, Avadi, Chennai-600 062, India sundarvtu@gmail.com
Institute of Technology, CMJ University Shillong, Meghalaya-793 003 India sivaperumals@gmail.com

Abstract. In this paper, new results based on the sliding mode control are derived for the global chaos synchronization of identical Coullet chaotic systems (1981). The stability results for the sliding mode control based synchronization schemes derived in this paper are established using Lyapunov stability theory. Since the Lyapunov exponents are not required for these calculations, the sliding mode control method is very effective and convenient to achieve global chaos synchronization of the identical Coullet chaotic systems. Numerical simulations are shown to illustrate the effectiveness of the sliding mode control results derived in this paper for the identical Coullet chaotic systems.

Keywords: Sliding mode control, global chaos synchronization, chaos, Coullet system.

1 Introduction

Chaotic systems are dynamical systems that are highly sensitive to initial conditions. This sensitivity is popularly known as the *butterfly effect* [1]. Since the pioneering work by Pecora and Carroll ([2], 1990), chaos synchronization problem has been studied extensively in the literature. Chaos theory has been applied to a variety of fields including physical systems [3], chemical systems [4], ecological systems [5], secure communications ([6]-[8]) etc.

In the last two decades, various control schemes have been developed and successfully applied for the chaos synchronization such as PC method [2], OGY method [9], active control ([10]-[12]), adaptive control ([13]-[15]), time-delay feedback method [16], backstepping design method ([17]-[18]), sampled-data feedback synchronization method ([19]-[20]) etc.

In most of the chaos synchronization approaches, the master-slave or drive-response formalism is used. If a particular chaotic system is called the master or drive system and another chaotic system is called the slave or response system, then the goal of the global chaos synchronization is to use the output of the master system to control the slave system so that the states of the slave system track the states of the master system asymptotically. In other words, global chaos synchronization is achieved when

the difference of the states of master and slave systems converge to zero asymptotically with time.

In this paper, we derive new results based on the sliding mode control ([21]-[23]) for the global chaos synchronization of identical Coullet systems ([24], 1981). The stability results for the sliding mode control based synchronization schemes derived in this paper are established using Lyapunov stability theory [25]. In robust control systems, sliding mode control is often adopted due to its inherent advantages of easy realization, fast response and good transient performance as well as its insensitivity to parameter uncertainties and external disturbances.

This paper has been organized as follows. In Section 2, we describe the problem statement and our methodology using sliding mode control. In Section 3, we discuss the global chaos synchronization of identical Coullet systems ([24], 1981). In Section 4, we summarize the main results obtained in this paper.

2 Problem Statement and Our Methodology Using Sliding Mode Control

In this section, we detail the problem statement for global chaos synchronization of identical chaos systems and our methodology using sliding mode control (SMC) and Lyapunov stability theory.

Consider the chaotic system described by

$$\dot{x} = Ax + f(x) \tag{1}$$

where $x \in \mathbb{R}^n$ is the state of the system, A is the $n \times n$ matrix of the system parameters and $f: \mathbb{R}^n \to \mathbb{R}^n$ is the nonlinear part of the system. We consider the system (1) as the *master* or *drive* system.

As the *slave* or *response* system, we consider the following chaotic system described by the dynamics

$$\dot{y} = Ay + f(y) + u \tag{2}$$

where $y \in \mathbb{R}^n$ is the state of the system and $u \in \mathbb{R}^m$ is the controller of the slave system.

If we define the synchronization error e as

$$e = y - x, (3)$$

then the error dynamics is obtained as

$$\dot{e} = Ae + \eta(x, y) + u$$
, where $\eta(x, y) = f(y) - f(x)$ (4)

The objective of the global chaos synchronization problem is to find a controller \boldsymbol{u} such that

$$\lim_{t \to \infty} \|e(t)\| = 0 \text{ for all initial conditions } e(0) \in \mathbb{R}^n$$
 (5)

To solve this problem, we first define the control u as

$$u(t) = -\eta(x, y) + Bv(t) \tag{6}$$

where B is a constant gain vector selected such that (A, B) is controllable.

Substituting (6) into (4), the error dynamics simplifies to

$$\dot{e} = Ae + Bv \tag{7}$$

which is a linear time-invariant control system with single input v.

Thus, the original global chaos synchronization problem can be replaced by an equivalent problem of stabilizing the zero solution e=0 of the linear system (7) be a suitable choice of the sliding mode control.

In the sliding mode control, we define the variable

$$s(e) = Ce = c_1e_1 + c_2e_2 + \dots + c_ne_n$$
 (8)

where $C = [c_1 \quad c_2 \quad \cdots \quad c_n]$ is a constant vector to be determined.

In the sliding mode control, we constrain the motion of the system (7) to the sliding manifold defined by

$$S = \{x \in \mathbb{R}^n \mid s(e) = 0\} = \{x \in \mathbb{R}^n \mid c_1 e_1 + c_2 e_2 + \dots + c_n e_n = 0\}$$

which is required to be invariant under the flow of the error dynamics (7).

When in sliding manifold S, the system (7) satisfies the following conditions:

$$s(e) = 0 (9)$$

which is the defining equation for the manifold S and

$$\dot{s}(e) = 0 \tag{10}$$

which is the necessary condition for the state trajectory e(t) of the system (7) to stay on the sliding manifold S.

Using (7) and (8), the equation (10) can be rewritten as

$$\dot{s}(e) = C\left[Ae + Bv\right] = 0\tag{11}$$

Solving (11), we obtain the equivalent control law given by

$$v_{eq}(t) = -(CB)^{-1}CAe(t) \tag{12}$$

where C is chosen such that $CB \neq 0$.

Substituting (12) into the error dynamics (7), we get the closed-loop dynamics as

$$\dot{e} = [I - B(CB)^{-1}C]Ae \tag{13}$$

where C is chosen such that the system matrix $[I - B(CB)^{-1}C]A$ is Hurwitz. Then the controlled system (13) is globally asymptotically stable. To design the sliding mode controller for the linear time-invariant system (7), we use the constant plus proportional rate reaching law

$$\dot{s} = -q \operatorname{sgn}(s) - ks \tag{14}$$

where $sgn(\cdot)$ denotes the sign function and the gains q > 0, k > 0 are determined such that the sliding condition is satisfied and sliding motion will occur.

From equations (11) and (14), we obtain the control v(t) as

$$v(t) = -(CB)^{-1}[C(kI + A)e + qsgn(s)]$$
(15)

Theorem 1. The master system (1) and the slave system (2) are globally and asymptotically synchronized for all initial conditions $x(0), y(0) \in \mathbb{R}^n$ by the feedback control law

$$u(t) = -\eta(x, y) + Bv(t) \tag{16}$$

where v(t) is defined by (15) and B is a column vector such that (A, B) is controllable. Also, the sliding mode gains k, q are positive.

Proof. First, we note that substituting (16) and (15) into the error dynamics (7), we obtain the closed-loop dynamics as

$$\dot{e} = Ae - B(CB)^{-1} [C(kI + A)e + q \operatorname{sgn}(s)]$$
(17)

To prove that the error dynamics (17) is globally asymptotically stable, we consider the candidate Lyapunov function defined by the equation

$$V(e) = \frac{1}{2} s^2(e)$$
 (18)

which is a positive definite function on \mathbb{R}^n .

Differentiating V along the trajectories of (17) or the equivalent dynamics (14), we obtain

$$\dot{V}(e) = s(e)\dot{s}(e) = -ks^2 - q\mathrm{sgn}(s) \tag{19}$$

which is a negative definite function on \mathbb{R}^n .

Thus, by Lyapunov stability theory [25], it is immediate that the error dynamics (17) is globally asymptotically stable for all initial conditions $e(0) \in \mathbb{R}^n$.

This completes the proof.

3 Global Chaos Synchronization of Identical Coullet Systems

3.1 Main Results

In this section, we apply the sliding mode control results obtained in Section 2 for the global chaos synchronization of identical Coullet systems ([24], 1981).

Thus, the master system is described by the Coullet dynamics

$$\dot{x}_1 = x_2
\dot{x}_2 = x_3
\dot{x}_3 = ax_1 - bx_2 - cx_3 - x_1^3$$
(20)

where x_1, x_2, x_3 are the states of the system and a > 0, b > 0, c > 0 are parameters of the system.

The slave system is also described by the Coullet dynamics

$$\dot{y}_1 = y_2 + u_1
\dot{y}_2 = y_3 + u_2
\dot{y}_3 = ay_1 - by_2 - cy_3 - y_1^3 + u_3$$
(21)

where y_1, y_2, y_3 are the states of the system and u_1, u_2, u_3 are the controllers to be designed.

The Coullet systems (20) and (21) are chaotic when a=5.5, b=3.5 and c=1.0. The chaotic portrait of the Coullet system is illustrated in Figure 1.

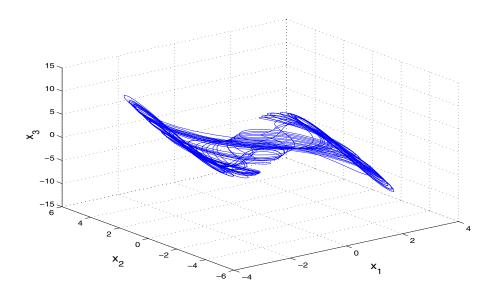


Fig. 1. Chaotic Portrait of the Coullet System

The chaos synchronization error e is defined by

$$e_i = y_i - x_i, \quad (i = 1, 2, 3)$$
 (22)

The error dynamics is easily obtained as

$$\dot{e}_1 = e_2 + u_1
\dot{e}_2 = e_3 + u_2
\dot{e}_3 = ae_1 - be_2 - ce_3 - y_1^3 + x_1^3 + u_3$$
(23)

We can write the error dynamics (23) in the matrix notation as

$$\dot{e} = Ae + \eta(x, y) + u \tag{24}$$

where the associated matrices are

$$A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ a - b - c \end{bmatrix}, \quad \eta(x, y) = \begin{bmatrix} 0 \\ 0 \\ -y_1^3 + x_1^3 \end{bmatrix} \quad \text{and} \quad u = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}$$
 (25)

The sliding mode controller design is carried out as detailed in Section 2.

First, we set u as

$$u = -\eta(x, y) + Bv \tag{26}$$

where B is chosen such that (A, B) is controllable. We take B as

$$B = \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix} \tag{27}$$

In the chaotic case, the parameter values are a = 5.5, b = 3.5 and c = 1.0.

The sliding mode variable is selected as

$$s = Ce = \begin{bmatrix} 10 & 4 & 1 \end{bmatrix} e \tag{28}$$

which makes the sliding mode state equation asymptotically stable.

We choose the sliding mode gains as k=1 and q=0.1. We note that a large value of k can cause chattering and an appropriate value of q is chosen to speed up the time taken to reach the sliding manifold as well as to reduce the system chattering.

From equation (15), we can obtain v(t) as

$$v(t) = -3.1e_1 - 2.1e_2 - 0.8e_3 - 0.02\operatorname{sgn}(s)$$
(29)

Thus, the required sliding mode controller is obtained as

$$u(t) = -\eta(x, y) + Bv(t) \tag{30}$$

where $\eta(x, y)$, B and v(t) are defined in equations (25), (27) and (29).

By Theorem 1, we obtain the following result.

Theorem 2. The identical Coullet systems (20) and (21) are globally and asymptotically synchronized for all initial conditions with the sliding mode controller u defined by (30).

3.2 Numerical Results

For the numerical simulations, the fourth-order Runge-Kutta method with time-step $h=10^{-6}$ is used to solve the Coullet systems (20) and (21) with the sliding mode controller u given by (30) using MATLAB.

For the Coullet systems, the parameter values are taken as those which result in the chaotic behaviour of the systems, viz.

$$a = 5.5, b = 3.5 \text{ and } c = 1.0$$

The sliding mode gains are chosen as

$$k = 1$$
 and $q = 0.1$

The initial values of the master system (20) are taken as

$$x_1(0) = 3$$
, $x_2(0) = 2$, $x_3(0) = 1$

and the initial values of the slave system (21) are taken as

$$y_1(0) = 1$$
, $y_2(0) = 5$, $y_3(0) = 4$

Figure 2 depicts the synchronization of the identical Coullet systems (20) and (21).

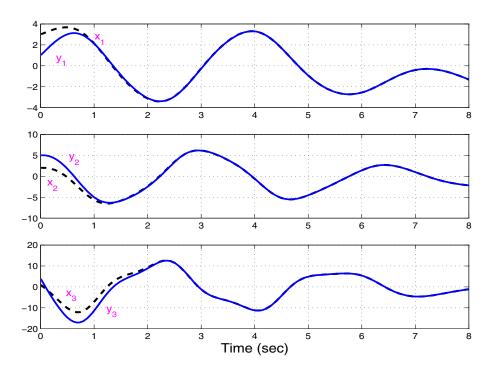


Fig. 2. Synchronization of the Identical Coullet Systems

4 Conclusions

In this paper, we have used sliding mode control (SMC) to achieve global chaos synchronization for the identical Coullet chaotic systems (1981). Our synchronization results for the identical Coullet chaotic systems have been established using Lyapunov stability theory. Since the Lyapunov exponents are not required for these calculations, the sliding mode control method is very effective and convenient to achieve global chaos synchronization for identical Coullet chaotic systems. Numerical simulations are also shown to illustrate the effectiveness of the synchronization results derived in this paper using sliding mode control.

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